

CERTIFICATE OF MAILING

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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

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|--------------|---|---|-------------------|------|
| Appln. No. | : | 10/006,535 | Confirmation No.: | 1081 |
| Applicant | : | FEDERICO CARNIEL et al. | | |
| Filed | : | December 5, 2001 | | |
| TC/A.U. | : | 3663 | | |
| Examiner | : | DEANDRA HUGHES | | |
| | | | | |
| Docket No. | : | CISCP735 | | |
| Customer No. | : | 26541 | | |
| Title | : | GAIN FLATTENED BI-DIRECTIONALLY PUMPED RAMAN AMPLIFIER FOR WDM TRANSMISSION SYSTEMS | | |

Commissioner for Patents
P.O. Box 1450
Alexandria, VA 22313-1450

DECLARATION OF ADA BRAVERMAN UNDER RULE 132

I, Ada Liva Braverman, an inventor of the above-identified patent application do declare as follows:

1. As will be explained, the invention of this patent application provides surprising results to a Raman amplification system by combining the use of N pumps in one pumping direction and N+1 pumps in the other pumping direction where the pump wavelengths alternate between directions.

2. The design of a Raman amplification system involves a complex set of tradeoffs. The Raman amplifier must provide sufficient gain to overcome losses along the span. Generally, the more gain that can be achieved, the greater the distance that can be achieved between optical amplification sites, directly affecting cost of the link. This gain should be achieved over a large bandwidth. The bandwidth of the amplifiers along a link determine how many channels can be carried, directly affecting link revenue.

3. The flatness of gain across the bandwidth is also a highly important figure of merit for Raman amplifiers. To satisfy receiver dynamic range requirements, it is necessary to have a flat gain response across the bandwidth. Flatness can be achieved by the use of gain flattening filters but these have an associated insertion loss that compromises the overall gain.

4. Achieving all of these objectives simultaneously is an enormous challenge. The designer can shift pump wavelengths and adjust pump powers to identify an optimal solution. However, improvements on one front often mean setbacks on another front. Reductions in gain variation across the band may be achieved only at the expense of overall gain. If pump power is increased arbitrarily in an effort to increase gain, there are undesired consequences such as nonlinear effects of gain saturation and four-wave-mixing between signal energy and pump energy.

5. Referring now to the table on page 1 of the Exhibit, simulation results are presented for five different configurations of pump wavelength and pump power. As in the example given at the bottom of page 12 of the present application, a gain of 23 dB is desired to compensate for the loss of a fiber span and multiplexers. The configuration of column 1 is in accordance with the present invention and employs two counter-propagating pump wavelengths and three co-propagating pump wavelengths while the configurations of columns 2-5 use two pump wavelengths of each type. Gain and gain deviation versus wavelength are plotted in Figs. 1-10 of the Exhibit.

6. It is apparent that configuration 1 achieves the desired 23.2 dB simultaneously with 1.2 dB of gain deviation using two co-propagating and three counter-propagating pumps. Configuration 2 represents an optimization of pump powers at the same four wavelengths to achieve the same gain flatness. As can be seen the 1.2 dB gain flatness can be achieved *but only at the expense of a 6.1 dB loss of gain*. This is a highly indicative point of comparison between embodiments of the present invention and the prior art. The 6.1 dB difference in average gain is a very large disparity. In the context of a real-world optical communication system, this would correspond to a loss of hundreds of kilometers, e.g., 1470 km instead of 2000 km, of available span length and a great increase in cost.

7. The remaining columns show configurations optimized to recover the lost gain by varying pump wavelengths and powers. Configuration 3 allows for optimization of pump wavelengths at the expense of shifting of the amplification window away from its target range.

Only half the lost gain is recovered but the gain deviation is doubled compared to what was achieved in configuration 1.

8. Configurations 4 and 5 increase the pump powers of the configuration of column 3 to recover the remaining lost gain. Configuration 5 exhibits 2.0 dB of gain deviation. There is however, a limit to the use of pump power increases to increase gain since undesired non-linear effects such as saturation and four-wave-mixing begin to appear.

9. The combination of gain and gain flatness provided by embodiments of the present invention represents a surprising result. The multiple objectives of gain, gain flatness, and bandwidth are achieved by relying on the features of the claimed invention including the use of N pumps in one pumping direction and N+1 pumps in the other pumping direction where the pump wavelengths alternate between directions.

The undersigned declarant declares further that all statements made herein of their own knowledge are true and all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States code and that such willful false statements may jeopardize the validity of the application or any patent issuing thereon.



Ada Liva Braverman

RITTER, LANG & KAPLAN LLP
12930 Saratoga Ave., Suite D1
Saratoga, CA 95070
Tel: 408-446-8690
Fax: 408-446-8691



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EXHIBIT

Simulation Results

| Configuration number | 1 | 2 | 3 | 4 | 5 |
|-------------------------------------|---------------|---------------|----------|----------|----------|
| Pump configuration | 2+3 | 2+2 | 2+2 | 2+2 | 2+2 |
| Total gain dev. | 1.2 | 1.2 | 2.4 | 2.4 | 2.0 |
| Min wavelength (nm) | 1572 | 1572 | 1579.6 | 1579.6 | 1578.2 |
| Max wavelength (nm) | 1617 | 1617 | 1624.6 | 1624.6 | 1623.2 |
| Bandwidth (nm) | 45 | 45 | 45 | 45 | 45 |
| Average Gain (dB) | 23.2 | 17.1 | 20.3 | 23.3 | 23 |
| Pump wavelength (nm) and power (mW) | 1455(ctp) 120 | 1455(ctp) - | - - - | - - - | - - |
| | 1472(ctp) 145 | 1472(ctp) 100 | 1470 145 | 1470 220 | 1470 230 |
| | 1509(ctp) 160 | 1509(ctp) 100 | 1513 160 | 1513 205 | 1513 195 |
| | 1463(cop) 215 | 1463(cop) 200 | 1459 215 | 1459 225 | 1459 235 |
| | 1499(cop) 225 | 1499(cop) 200 | 1501 225 | 1501 215 | 1501 205 |

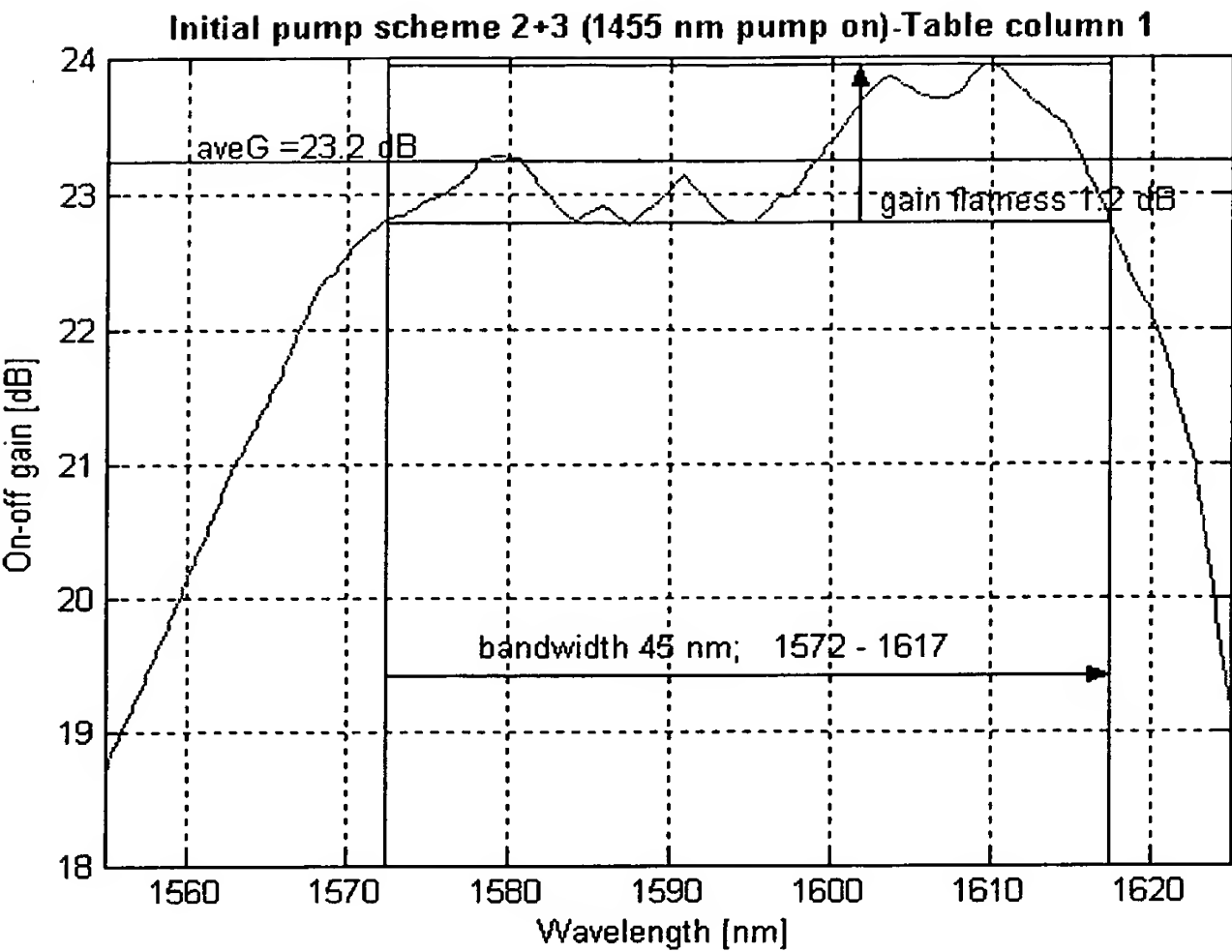


Fig. 1. On-off gain corresponding to the 2+3 pump scheme (column 1)

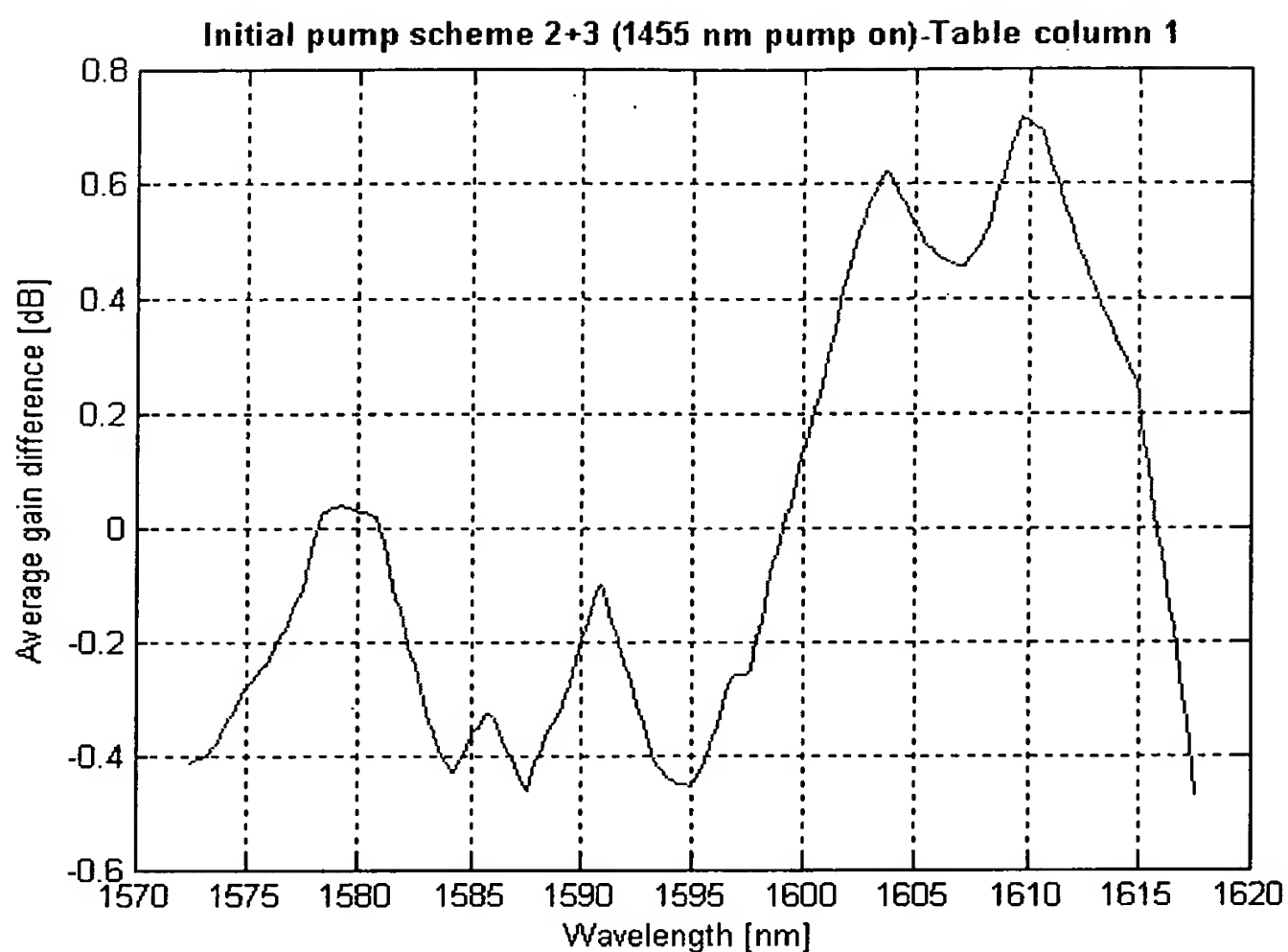


Fig. 2. Average gain deviation corresponding to the 2+3 pump scheme (column 1)

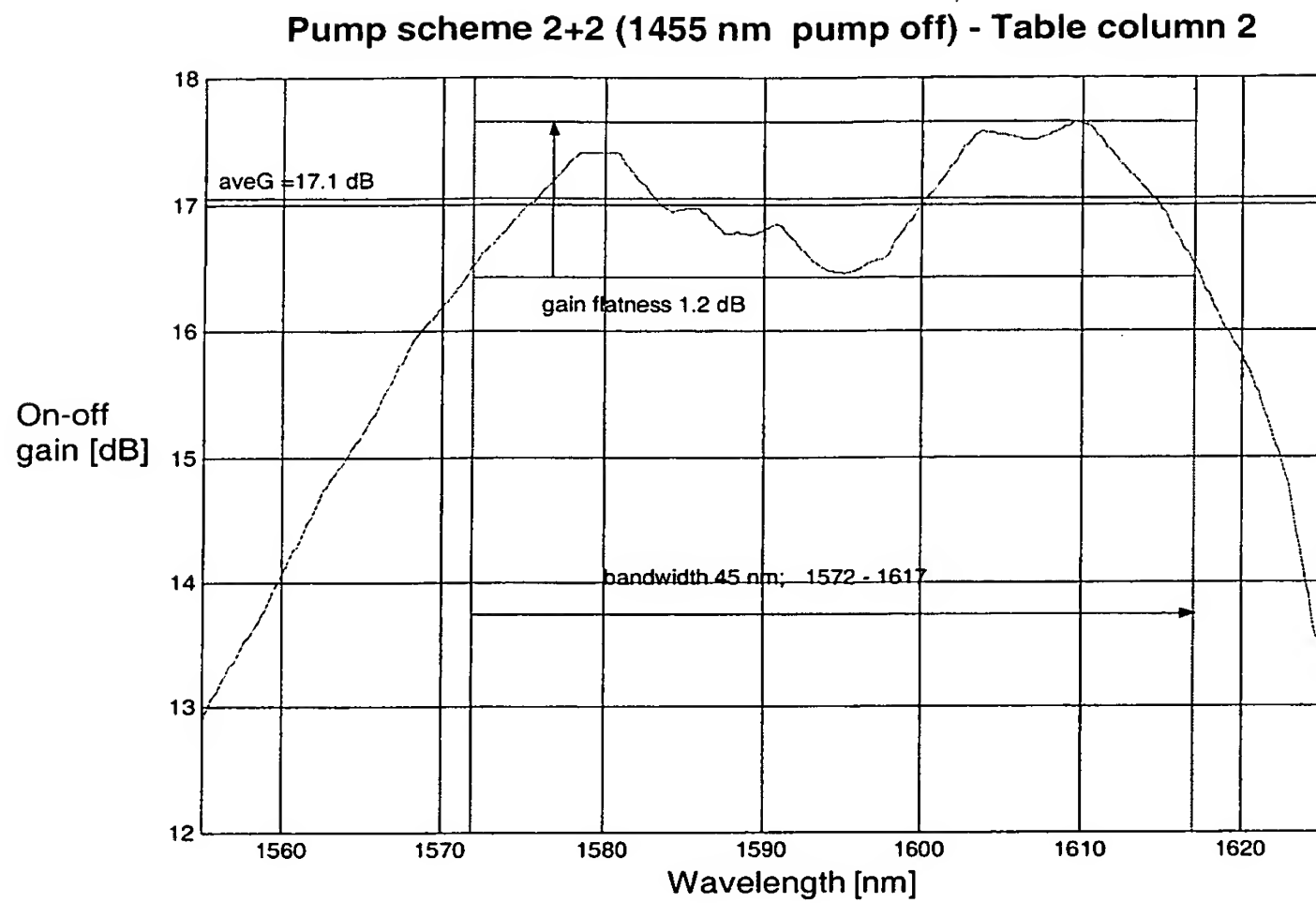


Fig. 3. On-off gain corresponding to the 2+2 pump scheme (column 2)

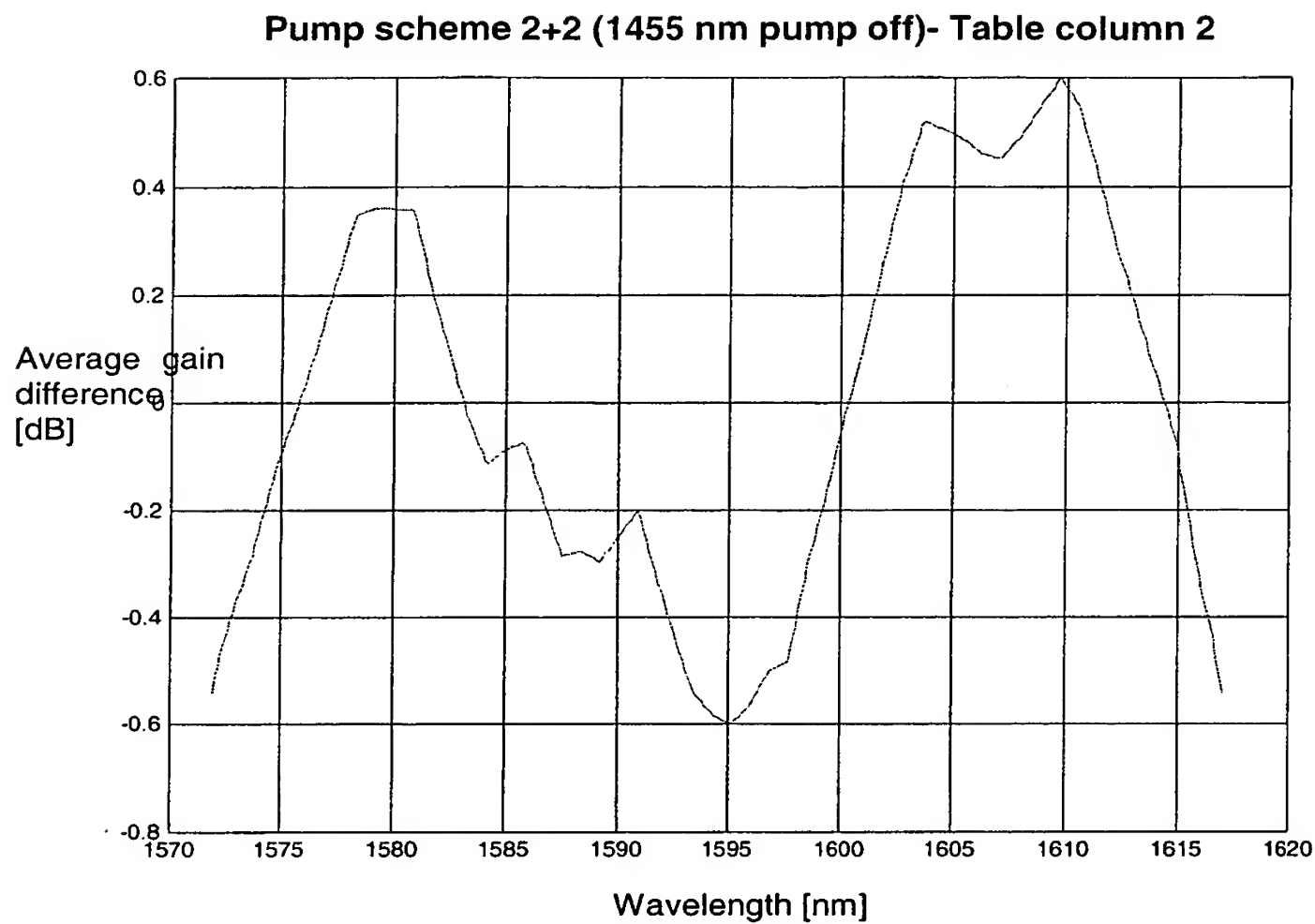


Fig. 4. Average gain deviation corresponding to the 2+2 pump scheme (column 2)

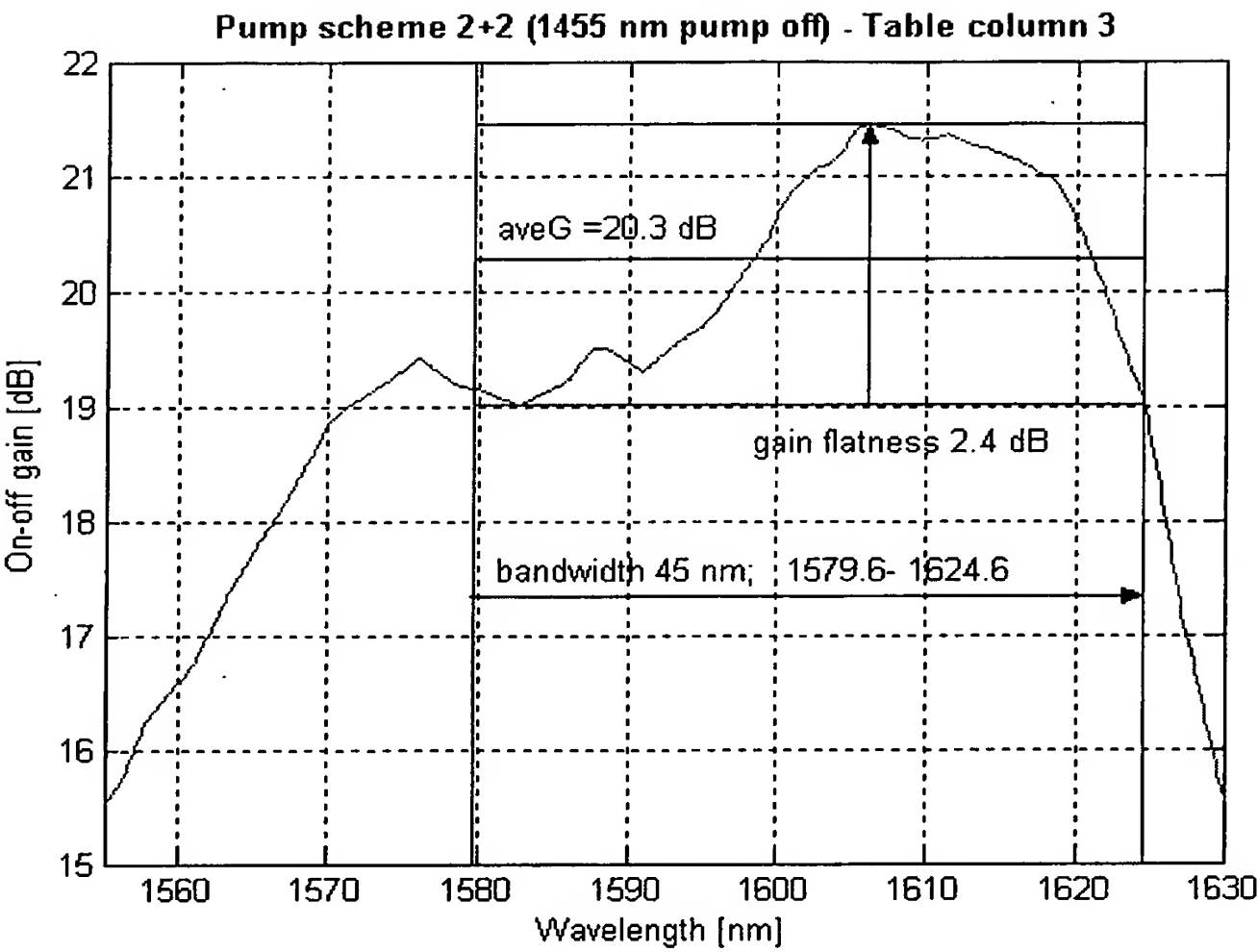


Fig. 5. On-off gain corresponding to the 2+2 pump scheme (column 3)

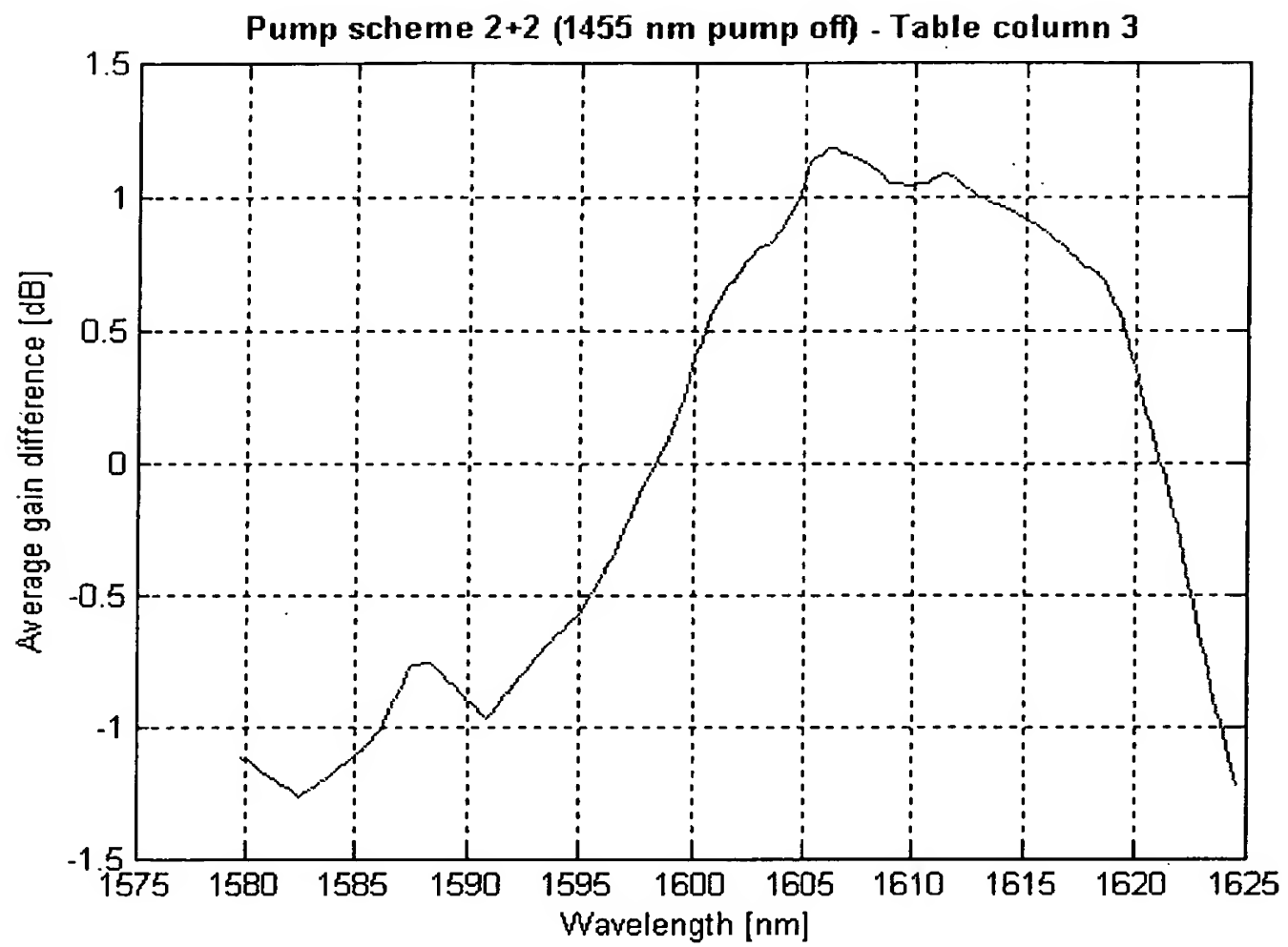


Fig. 6. Average gain deviation corresponding to the 2+2 pump scheme (column 3)

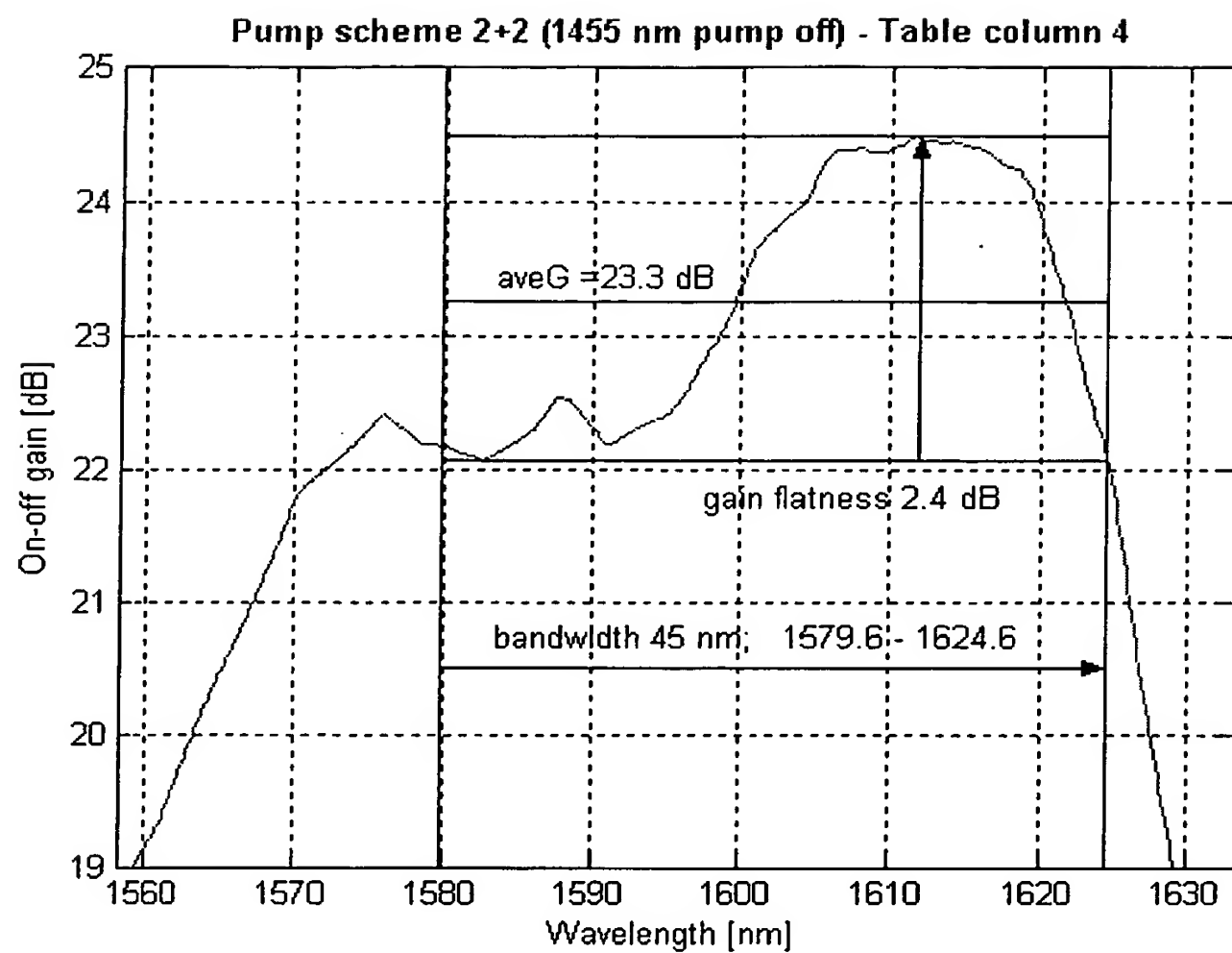


Fig.7. On-off gain corresponding to the 2+2 pump scheme (column 4)

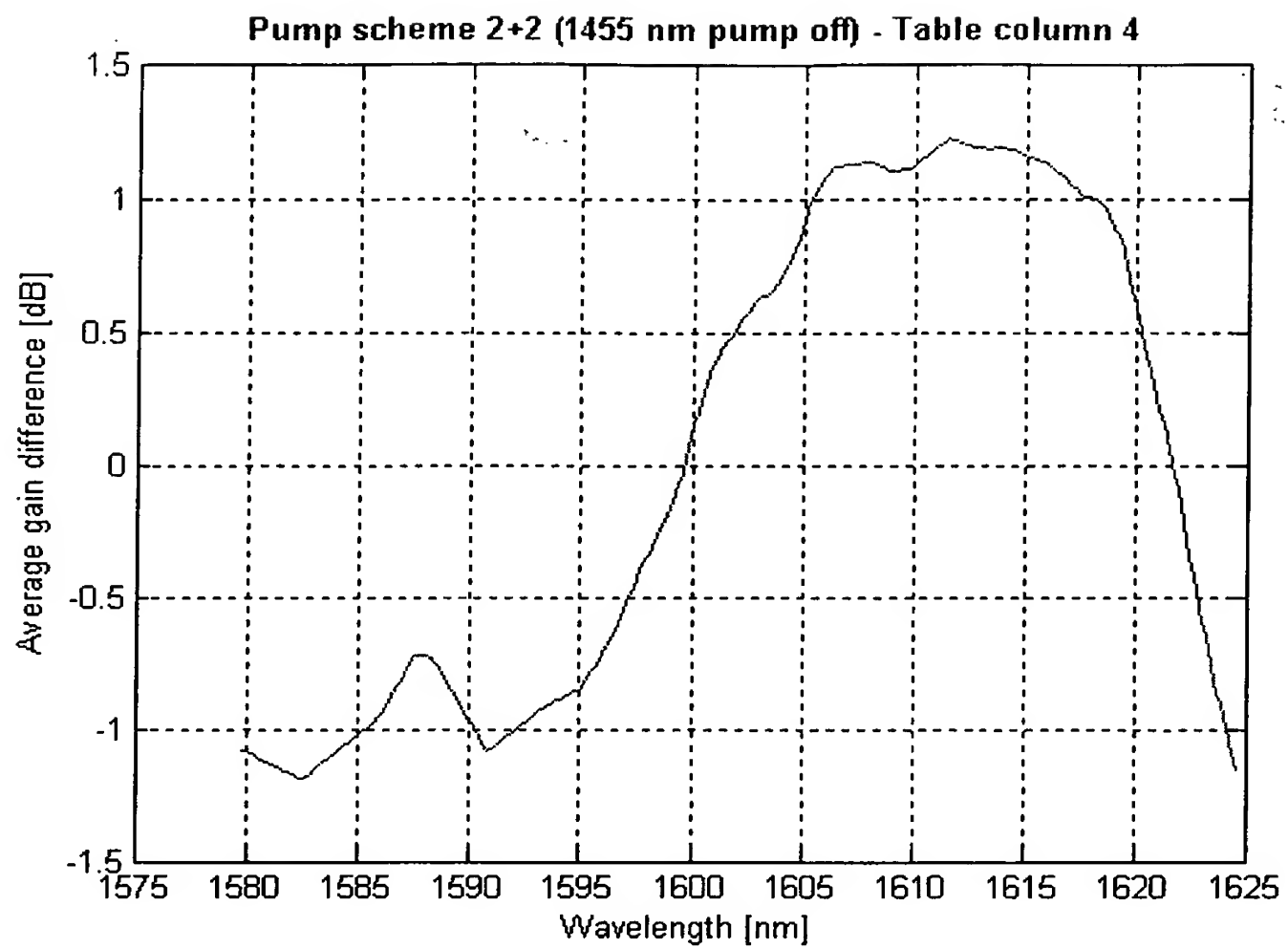


Fig. 8. Average gain deviation corresponding to the 2+2 pump scheme (column 4)

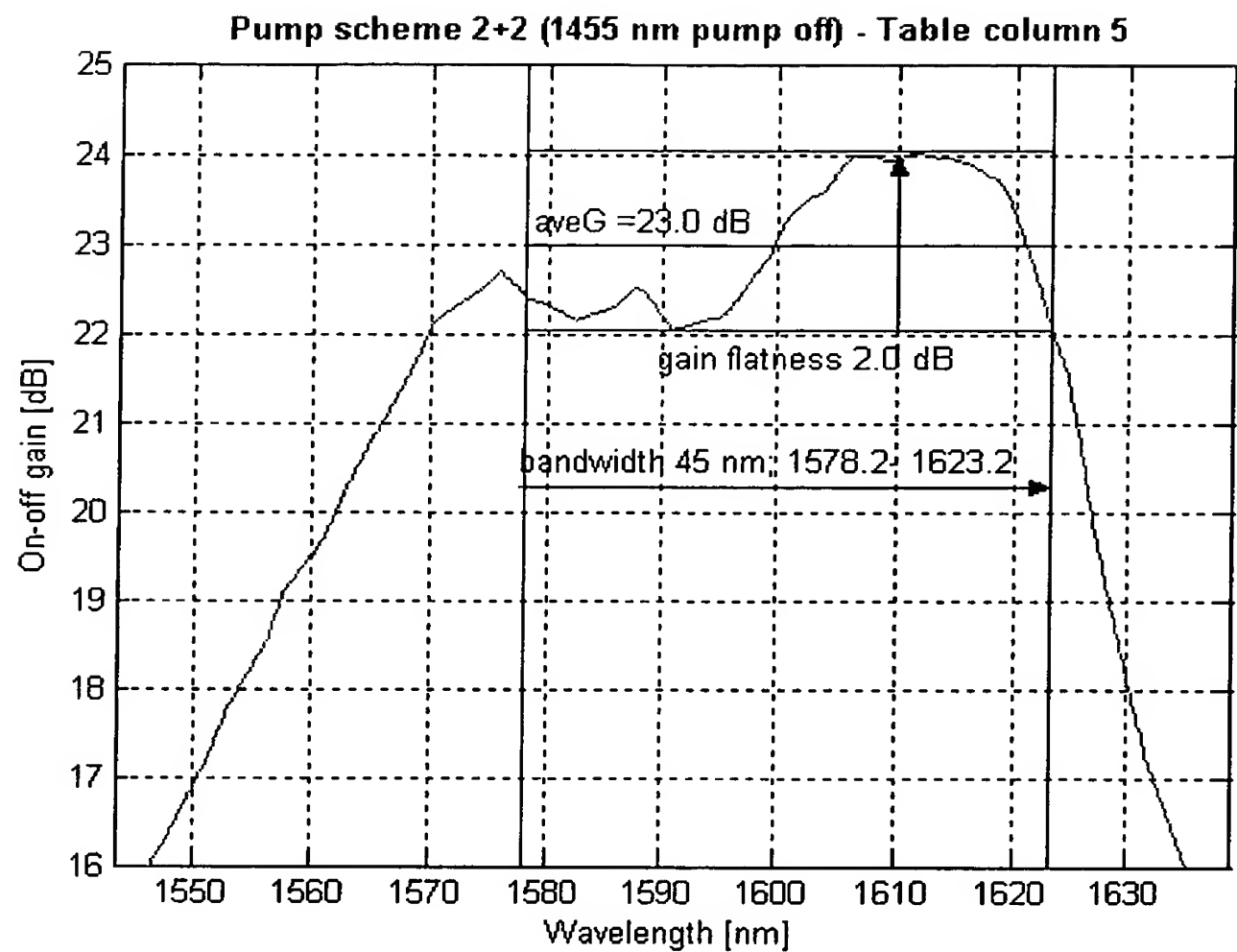


Fig.9. On-off gain corresponding to the 2+2 pump scheme (column 5)

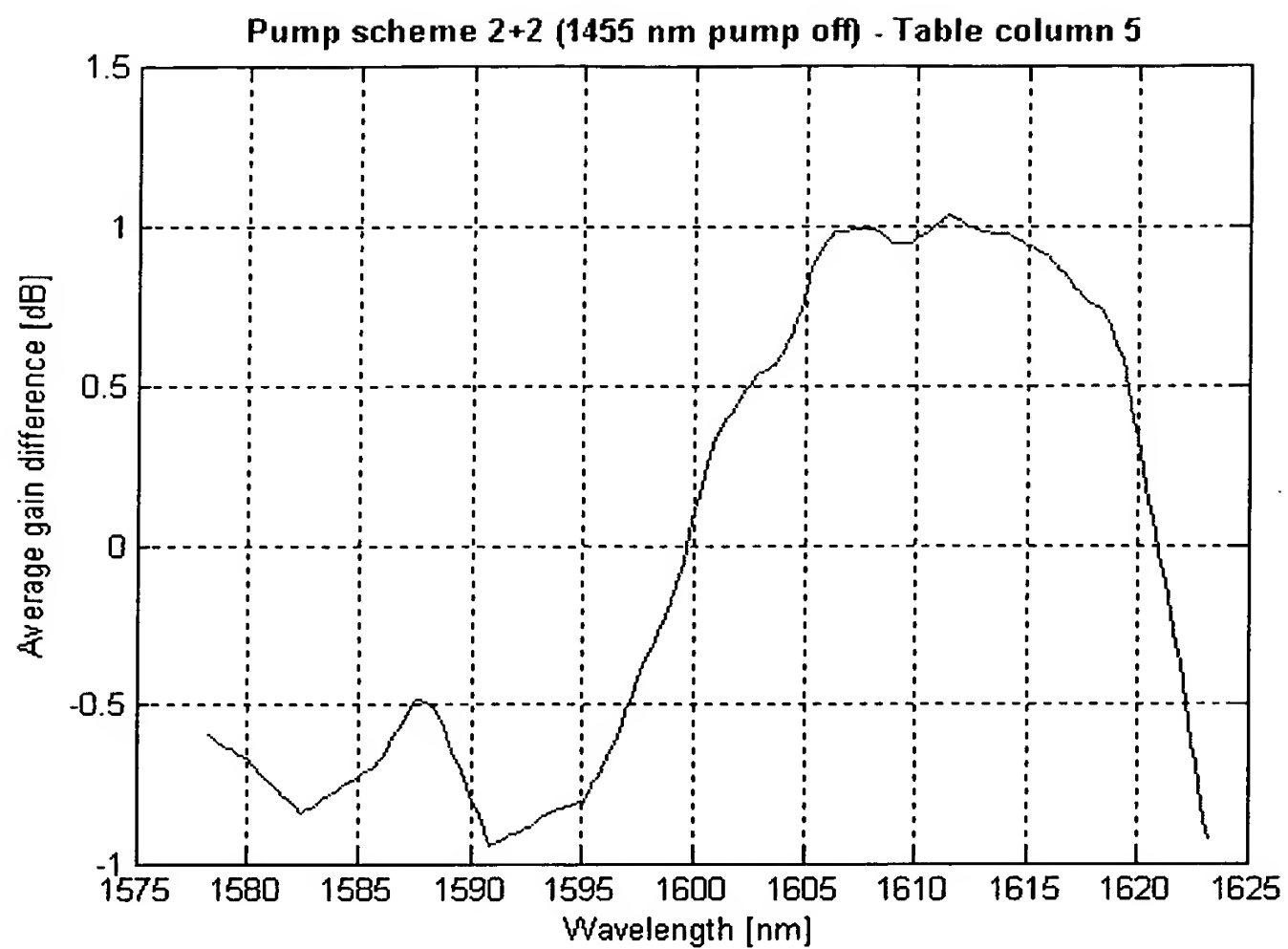


Fig. 10. Average gain deviation corresponding to the 2+2 pump scheme (column 5)